

GEOTECHNICAL ENGINEERING SERVICES REPORT NO. 1-40106

NM 4 WATERLINE REPLACEMENT

LOS ALAMOS COUNTY, NEW MEXICO

GEO-TEST, INC. 3204 RICHARDS LANE SANTA FE, NEW MEXICO 87507 (505) 471-1101 FAX (505) 471-2245

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PREPARED FOR:

LOS ALAMOS COUNTY DEPARTMENT OF PUBLIC UTILITIES



May 16, 2024 Job No. 1-40106

Los Alamos County **Department of Public Utilities** 1000 Central Ave., Suite 130 Los Alamos, NM 87544

Michelle Martinez ATTN:

RE: Geotechnical Engineering Services Report NM 4 Waterline Replacement Los Alamos County, New Mexico

Dear Ms. Martinez:

Submitted herein is the Geotechnical Engineering Services Report for the The report contains the results of our field above-referenced project. investigation, laboratory testing, and criteria pertaining to below grade utility installation.

It has been a pleasure to serve you on this project. If you should have any questions, please contact this office.

Respectfully submitted: GEO-TEST, INC.

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Patrick R. Whorton, PE

Reviewed By:

Patrick J. Byres, PE

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INTRODUCTION

This report presents the results of the geotechnical engineering services investigation performed by this firm for the proposed NM 4 Waterline Replacement project in Los Alamos, New Mexico.

The objectives of this investigation were to:

- 1) Evaluate the nature and engineering properties of the subsurface soils underlying the site.
- 2) Provide recommendations for subsurface utility installation including excavation and backfill criteria.

The investigation includes subsurface exploration, selected soil sampling, laboratory testing of the samples, performing an engineering analysis and preparation of this report.

PROPOSED CONSTRUCTION

It is understood that the project consists of the replacement of approximately 3 to 4 miles of water transmission line along NM 4. The new line will be installed approximately 4 feet below the existing roadway surface.

Should project details vary significantly from those outlined above, this firm should be notified for review and possible revision of the recommendations contained herein.

FIELD EXPLORATION

A total of four (4) exploratory borings were performed. Three (3) borings, Boring 6, 7 & 8 were drilled to a depth of 10 feet below existing surface grades. At the Boring 5 location at a depth of approximately 4 feet, the existing waterline was penetrated with the split spoon sampler. As shown in Photo 1 in a later section of this report, the existing waterline was not spotted in the correct location. After the line was hit at the Boring 5 location, the remaining borings, Boring 1, 2, 3, & 4 were not performed at the request of Los Alamos County.

Locations of the borings are shown on the attached Boring Location Map, Figure 1. The soils encountered in the completed borings were continuously examined, visually classified and logged during the drilling operation. The boring logs are presented in a following section of this report. Drilling was accomplished using a truck mounted drill rig equipped with 2.25-inch inner diameter hollow stem auger. Subsurface soils were sampled at five foot intervals or less utilizing an open tube split barrel sampler driven by a standard penetration test hammer.

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LABORATORY TESTING

Selected samples were tested in the laboratory to determine certain engineering properties of the soils. Moisture contents were determined to evaluate the various soil deposits with depth. The results of these tests are shown on the boring logs.

Sieve analysis and Atterberg limits tests were performed to aid in soil classification. The results of these tests are presented in the Summary of Laboratory Results and on the individual test reports presented in a following section of this report.

SURFACE CONDITIONS

A brief site reconnaissance was performed during our site exploration. The proposed waterline will be installed along NM 4 between White Rock and the East Jemez Rd. intersection. NM 4 is a two-lane asphalt paved roadway with existing subsurface utilities running beneath the shoulders. The roadway passes through Cedro Canyon, a relatively low-lying area bordered on either side by tuff bluffs.

SUBSURFACE SOIL CONDITIONS

As indicated by the exploratory borings the subsurface profile varied from each location explored.

At the Boring 5 location, above the existing waterline, medium dense low plasticity silty sand was encountered at the surface and extended to the waterline where the boring was terminated. This silty sand is processed fill primarily composed of weathered tuff.

At the Boring 6 location, very loose to loose low plasticity silt with sand was encountered and extended to the full depth explored. These soils are likely composed of some near surface man-made fill over deeper colluvial deposits of weathered tuff.

At the Boring 7 location, moderately firm low plasticity clayey sand was encountered at the surface and extended to a depth of 2 feet below surface grade where medium dense to dense non-plastic silty sand was encountered and extended to the full depth explored. These soils are likely composed of some near surface man-made fill over deeper colluvial deposits of weathered tuff.

At the Boring 8 location, moderately firm low plasticity clayey sand was encountered at the surface and extended to a depth of 2 feet below surface grade where medium dense low plasticity silty sand was encountered and

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extended to a depth of 6 feet below surface grade where firm non-plastic pumice was encountered and extended to a depth of 9 feet below surface grade where firm non-plastic weathered tuff was encountered and extended to the full depth explored.

No free groundwater was encountered in the borings and soil moisture contents were relatively low to moderate throughout the extent of the borings.

CONCLUSIONS AND RECOMMENDATIONS

As discussed in the previous section, the subsurface soils encountered along the proposed waterline alignment primarily consisted of natural colluvial deposits as well as man-made fills. Weak rock consisting of weathered tuff and pumice was encountered at the Boring 8 location.

Excavation of the subsurface soils throughout the site may be accomplished using normal earthmoving equipment and excavated soils may be reused as utility backfill given adequate processing to meet the specifications provided in the following section.

The existing near surface soils underlying the site classify as A-4 and A-2-4 according to the American Association of State Highway and Transportation Officials (AASHTO) soil classification system. According to the NMDOT, these soils possess correlated R-values ranging from 20 to 53 and are considered moderate to excellent subgrade soils for pavements.

Excavation of subsurface rock may also be accomplished with normal earthmoving equipment, although additional effort may be required. Based on the results of this investigation, difficult excavation is not anticipated, however, based on our experience in the area, hard tuff may be present along the alignment which may require the use of heavy ripping or rock breaking equipment to excavate. Although it is anticipated that a majority of the alignment may be excavated with normal earthmoving equipment, contractors should be prepared to utilize rock breaking equipment as required and at their discretion to complete the required excavations. Excavated tuff may be processed and reused and trench backfill, provided the resulting material meets the specifications included in the following section.

EXCAVATION & BACKFILL

Excavated slopes for foundation and utility construction should be designed and constructed in accordance with 29 CFR 1926, Subpart P, and any applicable state or local regulations. Excavated temporary slopes should not exceed 1.5 to 1 (horizontal to vertical). Shoring is recommended and should be designed by a qualified engineer utilizing the results of this investigation. Should additional soil data be required for shoring design; it may be provided

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by this firm upon request. Benching of temporary slopes may be conducted at the contractor's discretion provided all applicable safety standards are followed and the average slope is no steeper than 1.5:1.

Excavation of the onsite soils can be readily accomplished using normal earthmoving equipment. Areas of hard tuff may require additional effort.

All utility trench backfill should meet the fill specifications and should be placed according to the method outlined below:

- 1) The results of this investigation indicate that most of the onsite soils will be suitable for use as backfill, although some blending may be required to meet the specifications presented below. Any imported material must also meet the criteria for backfill.
- 2) All backfill should be free of vegetation and debris and contain no rocks larger than 3 inches. Gradation of the backfill material, as determined in accordance with ASTM D-422, should be as follows:

Size	Percent Passing
3 inch	100
No. 4	60 - 100
No. 200	5 - 60

- 3) The plasticity index of the structural fill should be no greater than 15 when tested in accordance with ASTM D-4318.
- 4) Bedding and pipe embedment materials to be used around the pipes should conform to the pipe manufacturer's recommendations and should be placed and compacted in accordance with project specifications, local requirements or governing jurisdiction.
- 5) All onsite soils are suitable for use as utility trench backfill provided, they are free of vegetation and debris and contain no rocks larger than 3 inches.
- 6) Structural fill and utility backfill, consisting of soils approved by the geotechnical engineer, shall be placed in 8 inch loose lifts and compacted with approved compaction equipment. Loose lifts should be reduced to 4 inches if handheld compaction equipment is used. All compaction of fill or backfill shall be accomplished to a minimum of 95 percent of the maximum dry density as determined in accordance with ASTM D-1557. The moisture content of the structural fill during compaction should be within 2 percent of the optimum moisture content.

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7) Tests for degree of compaction should be determined by the ASTM D-1556 method or ASTM D-6938. Observation and field tests should be carried on during fill and backfill placement by the geotechnical engineer to assist the contractor in obtaining the required degree of compaction. If less than 95 percent is indicated, additional compaction effort should be made with adjustment of the moisture content as necessary until 95 percent compaction is obtained.

REVIEW AND INSPECTION

This report has been prepared to aid in the evaluation of this site and to assist in the design of this project. It is recommended that the geotechnical engineer be provided the opportunity to review the final design drawings and specifications in order to determine whether the recommendations in this report are applicable to the final design. Review of the final design drawings and specifications should be noted in writing by the geotechnical engineer.

In order to permit correlation between the conditions encountered during construction and to confirm recommendations presented herein, it is recommended that the geotechnical engineer be retained to perform continuous observations and testing during the earthwork portion of this project.

CLOSURE

Our conclusions, recommendations and opinions presented herein are:

- 1) Based upon our evaluation and interpretation of the findings of the field and laboratory program.
- 2) Based upon an interpolation of soil conditions between and beyond the explorations.
- 3) Subject to confirmation of the conditions encountered during construction.
- 4) Based upon the assumption that sufficient observation will be provided during construction.
- 5) Prepared in accordance with generally accepted professional geotechnical engineering principles and practice.

This report has been prepared for the sole use of Los Alamos County specifically to aid in the design of the NM 4 Waterline Replacement project in Los Alamos County, New Mexico and not for use by any third parties without consent.

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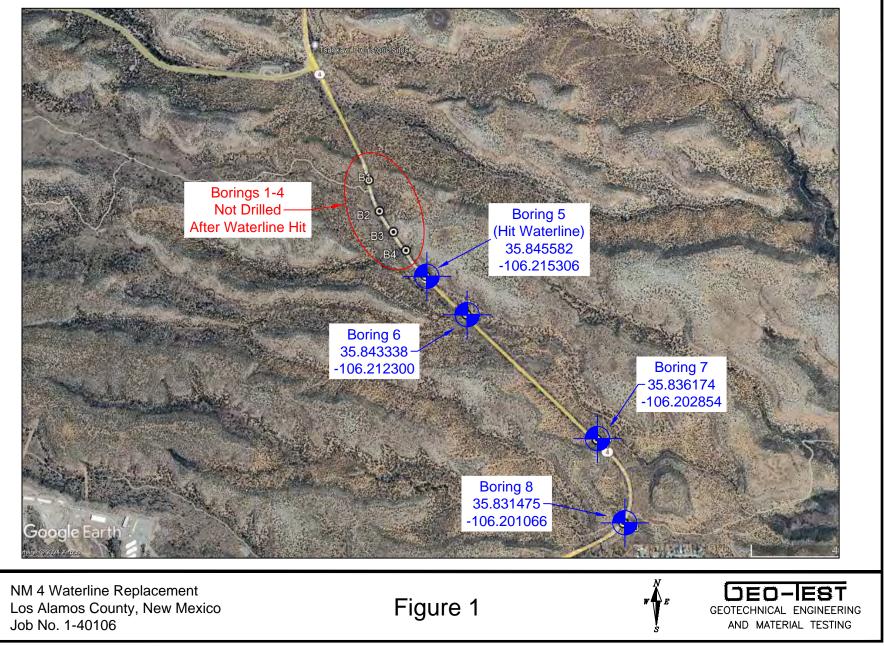
We make no other warranty, either expressed or implied. Any person using this report for bidding or construction purposes should perform such independent investigation as they deem necessary to satisfy themselves as to the surface and subsurface conditions to be encountered and the procedures to be used in the performance of work on this project. If conditions encountered during construction appear to be different than indicated by this report, this office should be notified.

All soil samples will be discarded 60 days after the date of this report unless we receive a specific request to retain the samples for a longer period of time.

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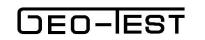
BORING LOCATION MAP





NM 4 Waterline Replacement Los Alamos, New Mexico Job No. 1-40106 Ruptured Waterline @ Boring 5 Photo 1





NM 4 Waterline Replacement Project: 04/16/2024 Project No: 1-40106 Date: Elevation: Type: 2.25" ID HSA

LOG OF TEST BORINGS

GROUNDWATER DEPTH

NO: 5

During Drilling: none

After 24 Hours:

Γ	SAMPLE								SUBSURFACE PROFILE	
	DEPTH (Ft)	POG	SAMPLE INTERVAL	ТҮРЕ	N. BLOWS/FT	MOISTURE %	DRY DENSITY (pcf)	usc	DESCRIPTION	N blows/ft 20 40 60 80
	-		\times	SS SS	7-8-9 17 3-3-0 3	15		SM	SILTY SAND, low plasticity, medium dense, moist, brown	
	5 —								Stopped Auger @ 2.5 feet Hit existing WATERLINE with sampler @ 4 feet - halted drilling operation	
I GEO TEST.GDT 5/15/24	- - 10 —									
LOG OF TEST BORING 1-40106.GPJ GEO TEST.GDT 5/15/24	- - 15 —	-								

LEGEND

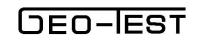
SS - Split Spoon
AC - Auger Cuttings
UD/SL - Undisturbed Sleeve

AMSL - Above Mean Sea Level

CS - Continuous Sampler

UD - Undisturbed

ST - Shelby Tube Stratification lines represent approximate boundaries between soil types. Transitions may be gradual. Water level readings have been made at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurments were made.



Project:NM 4 Waterline ReplacementDate:04/16/2024Project No:1-40106Elevation:Type:2.25" ID HSA

LOG OF TEST BORINGS

GROUNDWATER DEPTH

NO: 6

During Drilling: none

After 24 Hours:

Γ					SA	MPLE			SUBSURFACE PROFILE			
	DEPTH (Ft)	POG	SAMPLE INTERVAL	ТҮРЕ	N. BLOWS/FT	MOISTURE %	DRY DENSITY (pcf)	USC	DESCRIPTION	20	N blows/ft 40 60	80
	-			SS	2-1-2 3	10				¶3		
15/24	-		$\left \right\rangle$	SS	2-3-4 7	7					$ \begin{array}{c} \cdot \\ \cdot \\$	
	5 —		\square	SS	2-3-3 6	6		ML	SILT with SAND, low plasticity, very loose to loose, moist to slightly moist, light brown to purpleish brown			
	-			SS	2-1-2 3	6				•3		
TEST.GDT	10 —		SS 2-2-2 6			4		, , , , , , ,				
LOG OF TEST BORING 1-40106.GPJ GEO TEST.GDT 5/15/24	-								Stopped Auger @ 9 feet Stopped Sampler @ 10.5 feet			
OG OF TEST	- 15 —										$ \begin{array}{c} \cdot \begin{array}{c} \cdot \\ \end{array} \\ \end{array} \\ \end{array} \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ $	

LEGEND

SS - Split Spoon	
AC - Auger Cuttings	

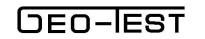
UD/SL - Undisturbed Sleeve

AMSL - Above Mean Sea Level

CS - Continuous Sampler

UD - Undisturbed

Stratification lines represent approximate boundaries between soil types. Transitions may be gradual. Water level readings have been made at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurments were made.



NM 4 Waterline Replacement Project: 04/16/2024 Project No: 1-40106 Date: Elevation: Type: 2.25" ID HSA

LOG OF TEST BORINGS

GROUNDWATER DEPTH

NO: 7

During Drilling: none

After 24 Hours:

Γ					SAI	MPLE			SUBSURFACE PROFILE	
	DEPTH (Ft)	DOJ	SAMPLE INTERVAL	ТҮРЕ	N. BLOWS/FT	MOISTURE %	DRY DENSITY (pcf)	usc	DESCRIPTION	N blows/ft 20 40 60 80
-	-			SS	3-5-4 9	18		SC	CLAYEY SAND, low plasticity, moderately firm, very moist, dark brown	
	-			SS	7-12-13 25	10				
	5 —		\times	SS	9-13-20 33	12				
	-			SS	12-15-20			SM	SILTY SAND, non-plastic, medium dense to dense, moist, brown to light brown	
GDT 5/15/24	-		\square		35	/				
LOG OF TEST BORING 1-40106.GPJ GEO TEST.GDT 5/15/24	10 —		\wedge	SS	14-10-14 24	9			Stopped Auger @ 9 feet Stopped Sampler @ 10.5 feet	
30RING 1-40106	-	-								
LOG OF TEST E	- 15 —	-								

LEGEND

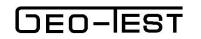
SS - Split Spoon
AC - Auger Cuttings
UD/SL - Undisturbed Sleeve

AMSL - Above Mean Sea Level

CS - Continuous Sampler

UD - Undisturbed

ST - Shelby Tube Stratification lines represent approximate boundaries between soil types. Transitions may be gradual. Water level readings have been made at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurments were made.



Project: NM 4 Waterline Replacement 04/16/2024 Date: Project No: 1-40106 Elevation: Type: 2.25" ID HSA

LOG OF TEST BORINGS

GROUNDWATER DEPTH

NO: 8

During Drilling: none

After 24 Hours:

Γ					SAM	MPLE			SUBSURFACE PROFILE		
	DEPTH (Ft)	POG	SAMPLE INTERVAL	ТҮРЕ	N. BLOWS/FT	MOISTURE %	DRY DENSITY (pof)	USC	DESCRIPTION		N lows/ft 0 60 80
	-		\square	SS	14-11-8 19	11		SC	CLAYEY SAND, low plasticity, moderately firm, moist, dark brown	<u>1</u> 19	
	- - 5 —		$\left \right\rangle$	SS SS	4-6-8 14 9-9-12 21	14 13		SM	SILTY SAND, low plasticity, medium dense, moist, light brown		
/15/24	-			SS	7-8-10 18	12		SW-SM	WELL GRADED SAND with SILT (pumice), non-plastic, firm, moist, blueish gray	18	
06.GPJ GEO TEST.GDT 5	10 —	-	\mathbf{X}	SS	12-12-10 22	12		TUFF	WEATHERED TUFF, non-plastic, firm, moist, light brown Stopped Auger @ 9 feet Stopped Sampler @ 10.5 feet	22.	
LOG OF TEST BORING 1-40106.GPJ GEO TEST.GDT 5/15/24	- - 15 —	-									

LEGEND

SS - Split Spoon	
AC - Auger Cuttings	

UD/SL - Undisturbed Sleeve

AMSL - Above Mean Sea Level

CS - Continuous Sampler

UD - Undisturbed

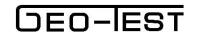
ST - Shelby Tube Stratification lines represent approximate boundaries between soil types. Transitions may be gradual. Water level readings have been made at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurments were made.

SUMMARY OF LABORATORY RESULTS

						SIEVE ANALYSIS PERCENT PASSING											
TEST HOLE	DEPTH (FEET)	UNIFIED CLASS	(%) MOIST	LL	PI	NO 200	NO 100	NO 40	NO 10	NO 4	3/8"	1/2"	3/4"	1"	1 1/2"	2"	4"
5	1.0	SM	14.9	28	1	35	47	60	94	97	98	100					
6	1.0		9.5														
6	3.0		7.2														
6	5.0	ML	6.2	28	1	74	84	92	98	100							
6	8.0		6.5														
6	10.0		6.3														
7	1.0		18.3														
7	3.0	SC	9.5	32	10	48	71	82	99	100							
7	5.0		12.1														
7	8.0	SM	7.2	NP	NP	18	37	59	95	99	100						
7	10.0		8.8														
8	1.0		11.1														
8	3.0	SM	14.2	29	3	38	59	73	94	96	99	100					
8	5.0		13.4														
8	8.0	SW-SM	11.6	NP	NP	9	14	28	83	93	97	98	100				
8	10.0		11.5														
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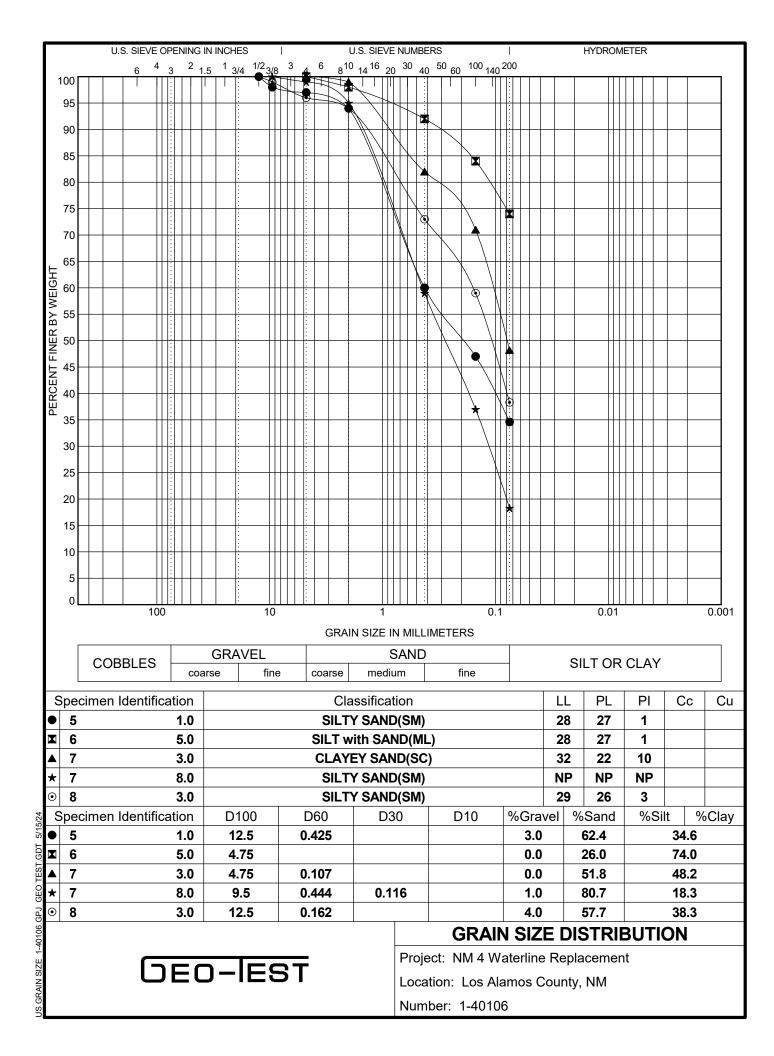
Sheet 1 of 1

	Sheet 1														
Borehole	Depth	Liquid Limit	Plastic Limit	Plasticity Index	Maximum Size (mm)	%<#200 Sieve	Class- ification	Water Content (%)	Dry Density (pcf)	AASHTO CLASS	Corr. R-Value				
5	1.0	28	27	1	12.5	35	SM	14.9		A-2-4	53				
6	1.0							9.5							
6	3.0							7.2							
6	5.0	28	27	1	4.75	74	ML	6.2		A-4	43				
6	8.0							6.5							
6	10.0							6.3							
7	1.0							18.3							
7	3.0	32	22	10	4.75	48	SC	9.5		A-4	20				
7	5.0							12.1							
7	8.0	NP	NP	NP	9.5	18	SM	7.2		A-2-4	55				
7	10.0							8.8							
8	1.0							11.1							
8	3.0	29	26	3	12.5	38	SM	14.2		A-4	38				
8	5.0							13.4							
8	8.0	NP	NP	NP	19	9	SW-SM	11.6		A-1-b	69				
8	10.0							11.5							



Summary of Laboratory Results

Project: NM 4 Waterline Replacement Location: Los Alamos County, NM Number: 1-40106



Г			U.\$	S. SIE	VE	OPI				INCHES					U.S. SIEVE N														HYDROMETER																				
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	GRAIN SIZE IN MILLIMETERS																																																
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	L			02					ars	rse fine					coarse				mediur			<u>m</u>																											
Specimen Identification									Classificatio										۱								LL PL				PI			Сс	Cu														
● 8 8.0								WELL-GRADED SAND w										/ith	ith SILT(SW-SM)								NP		NP)	1	NP		2.13	11.5														
S	Specimen Identification D100 D60										D3	0	D D1			010	10 %Gra			ave	vel %Sand		k	%Silt %Clay																									
	● 8 8.0								19					1.047				0.4					0.0		091		7.			84		4.5				8.5													
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